

Visible & Infrared Survey Telescope for Astronomy

## Data Flow System

**Document Title:** VISTA Infra Red Camera DFS System Impact

**Document Number:** VIS-SPE-IOA-20000-0001

**Issue:** 1.2

**Date:** 2005-05-09

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## Change Record

Issue	Date	Sections Affected	Description of Change/Change Request Reference/Remarks
0.5	2004-04-08	All	New document
1.0	2004-12-15	All	FDR release
1.1	2005-02-08	All	post-FDR revision
1.2	2005-05-09	ref,4	new ESO docs referenced, Data rates revised

## Notification List

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## 1 Introduction

The Visible and Infrared Survey Telescope for Astronomy (VISTA) is a new 4-metre telescope designed specifically for imaging survey work at visible and near-infrared wavelengths. The pawprint of the VISTA infrared camera (VIRCAM) will cover  $0.59 \text{ degree}^2$  in YJHK<sub>s</sub> passbands, using a 4×4 array of 2k×2k non-butable chips with ~0.34" pixels. A visible camera may be added in future.

One of the main design drivers for VISTA was to maximise the observing efficiency and sensitivity for large area surveys. The Science Requirements for VISTA are detailed in the VISTA Science Requirements Document [RD3]. For design purposes a set of surveys were defined in the Operational Concepts Definition Documents [RD5]. These can be briefly described as surveys which are very deep over a small area, medium deep over a medium area, and shallow over a wide area.

VISTA will be located in the southern hemisphere, at the European Southern Observatory's (ESO's) Cerro Paranal Observatory.

### 1.1 Scope of this Document

The optimization of scientific return from VISTA will depend crucially on the complete specification of the data flow from detector to final astrophysical data product. Standardization of observing modes, by means of the specification of observing protocols, will ensure that all necessary and sufficient calibration data are obtained to support science frames at maximum efficiency. The observing modes and the science goals have been used to place overall requirements on the VISTA pipeline, which are outlined in this document.

In summary, the VISTA data pipeline must provide Data Quality Control (DQC) measures, remove the instrumental signature from the raw data, and perform precision photometric and astrometric calibration.

This document was originally released under the title "VISTA Infra Red Camera DFS User Requirements" in compliance with issue 1.0 of [AD1] and has been renamed and revised following ESO review [RD11].

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## 1.2 Applicable Documents

[AD1] *Data Flow for the VLT/VLTI Instruments Deliverables Specification*, VLT-SPE-ESO-19000-1618, issue 2.0, 2004-05-22.

## 1.3 Reference Documents

- [RD1] *VISTA Infra Red Camera DFS Calibration Plan*, VIS-SPE-IOA-20000-00002, issue 1.1, 2005-04-28.
- [RD2] *VISTA Infra Red Camera DFS Data-Reduction Specifications*, VIS-SPE-IOA-20000-00003, issue 1.0, 2004-12-15.
- [RD3] *VISTA Science Requirements Document*, VIS-SPE-VSC-00000-0001, issue 2.0, 2000-10-26
- [RD4] *VISTA IR Camera Technical Specification*, VIS-SPE-ATC-06000-0004 Issue 2.0
- [RD5] *VISTA Operational Concept Definition Document*, VIS-SPE-VSC-00000-0002 issue 1.0, 2001-03-28
- [RD6] *VISTA Observing Efficiency Budget*, VIS-TRE-ATC-00002-0009, issue 1.0, 2001-09-27.
- [RD7] *VISTA Infrared Camera Data Flow System PDR RID Responses*, VIS-TRE-IOA-20000-0006 issue 1.0
- [RD8] *VISTA Infrared Camera Data Flow System Exposure Time Calculator*, VIS-SPE-IOA-20000-0009, Issue 1.0, 2004-12-15.
- [RD9] *Survey Definition Tool and Survey Progress Tools: Functional Specification*, VIS-SPE-ATC-20500-0001, Issue 1.0
- [RD10] *Requirements for Surveys: Planning, Scheduling and Progress*, VIS-SPE-QMU-20000-0007, Issue 1.0, 17 June 2004.
- [RD11] *VISTA Infrared Camera Data Flow System FDR RID Responses*, VIS-TRE-IOA-20000-0013

## 1.4 Abbreviations and Acronyms

2MASS	2-Micron All Sky Survey
AO	Adaptive Optics (not aO, active optics)
aO	active Optics (not AO, adaptive optics)
CDS	Correlated Double Sampling
DAS	Data Acquisition System
DFS	Data Flow System
ETC	Exposure Time Calculator
FITS	Flexible Image Transport System
ICRS	International Coordinate Reference System
LOWFS	Low Order Wave-Front Sensor
OB	Observation Block
OT	Observing Tool
PSF	Point Spread Function

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QC-0	Quality Control, level zero
QC-1	Quality Control, level one
SNR	Signal to Noise Ratio
SRD	Science Requirements Document
TCS	Telescope Control System
USNOB	US Naval Observatory All-Sky Photographic Catalogue
VDFS	VISTA Data Flow System
VIRCAM	VISTA Infrared Camera
VISTA	Visible and Infrared Survey Telescope for Astronomy
WCS	World Coordinate System
WFCAM	Wide Field Camera (on UKIRT)

## 1.5 Glossary

<b>Confidence Map</b>	An integer array, normalized to a median of 100% which is associated with an image. Combined with an estimate of the sky background variance of the image it assigns a relative weight to each pixel in the image and automatically factors in an exposure map. Bad pixels are assigned a value of 0. It is especially important in image filtering, mosaicing and stacking.
<b>Exposure</b>	The stored product of many individual <b>integrations</b> , which have been co-added in the DAS. Each exposure is associated with an exposure time.
<b>Integration</b>	A simple snapshot, within the DAS, of a specified elapsed time. This elapsed time is known as the integration time.
<b>Jitter (pattern)</b>	A pattern of <b>exposures</b> at positions each shifted by a small <b>movement</b> (<30 arcsec) from the reference position. Unlike a <b>microstep</b> the non-integral part of the shifts is any fractional number of pixels. Each position of a jitter pattern can contain a <b>microstep</b> pattern.
<b>Microstep (pattern)</b>	A pattern of <b>exposures</b> at positions each shifted by a very small <b>movement</b> (<3 arcsec) from the reference position. Unlike a <b>jitter</b> the non-integral part of the shifts are specified as 0.5 of a pixel (i.e. shift is N+0.5 pixel), which allows the pixels in the series to be interleaved in an effort to increase resolution. A microstep pattern can be contained within each position of a <b>jitter</b> pattern.
<b>Movement</b>	A change of position of the telescope that is not large enough to require a new guide star.
<b>Offset</b>	A change of position of the telescope that is not large enough to require a telescope <b>preset</b> , but is large enough to require a new guide star.
<b>Pawprint</b>	The 16 non-contiguous images of the sky produced by the

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VISTA IR camera, with its 16 non-contiguous chips (see Figure 2-1). The name is from the similarity to the prints made by the padded paw of an animal (the analogy suits earlier 4-chip cameras better).

**Pipeline**

a number of software components through which data flows automatically, processing raw frames into calibrated products.

**Preset**

A telescope slew to a new position involving a reconfiguration of the telescope control system and extra housekeeping operations that are not necessary for a **movement** or an **offset**.

**Tile**

A filled and fully sampled area of sky formed by combining multiple **pawprints**. Because of the detector spacing, the minimum number of pointed observations (with fixed offsets) required for reasonably uniform coverage is 6, which would expose each piece of sky, away from the edges of the tile, to at least 2 camera pixels. The pipeline does not combine **pawprints** into tiles.

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## 2 Telescope and Instrument Overview

### 2.1 General Layout

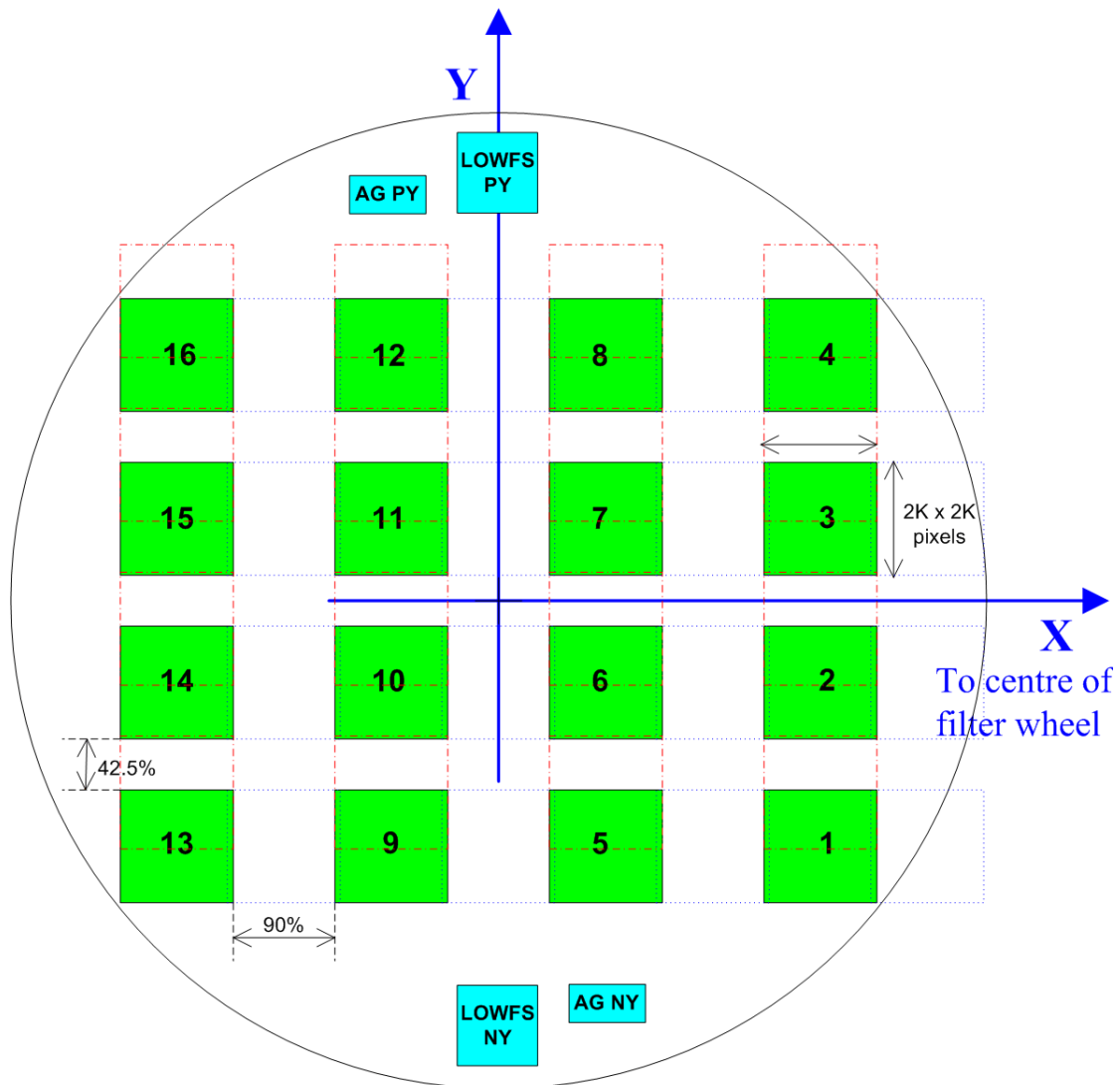
VISTA is an alt-azimuth 2-mirror telescope with a single focal station (Cassegrain) which can accommodate one of two possible cameras: an IR Camera or (if funded later) a visible camera. The telescope has a fast focal ratio (f/1 primary, f/3.25 at Cass) hence a compact structure. The telescope uses active optics, with 84 axial force actuators controlling the shape of the primary mirror (M1), and a 5-axis hexapod controlling the position of the secondary mirror (M2).

The infrared camera (details in [RD4]) is a novel design with no cold stop, but instead a long cold baffle extending  $\sim 2.1\text{m}$  above the focal plane to minimise the detectors' view of warm surfaces. There is a large entrance window (95cm diameter) and 3 corrector lenses, all IR-grade fused silica. There is only one moving part (the filter wheel). The camera also contains fixed autoguiders and wavefront sensors (2 each, using CCDs operating at  $\sim 800\text{nm}$  wavelength) to control the tracking and active optics. Table 2-1 gives approximate values for the main system parameters.

Telescope Mount	Alt-Azimuth
Focal Station	Cassegrain
Primary Mirror Diameter	4.1 metre
Entrance Pupil Diameter	3.7 metre
Secondary Mirror Diameter	1.24 metre
Baffle Diameter	1.63 metre
System Focal Length	12.072 metre
Wavelength Range	0.85-2.4 $\mu\text{m}$
Field of View (total)	1.65° diameter
Field of View (detectors)	0.59 deg <sup>2</sup> (1.5°×1° tiled)
Detectors	4×4 mosaic of 2048×2048 Raytheon VIRGO
Pixel Scale (Infrared)	0.34" / 20 $\mu\text{m}$
Controllers	ESO IRACE
System Image Quality	$\leq 0.5''$ (goal: 0.4").
Readouts	16 per detector (each a "stripe" of 2048×128 pixels).
Readout time	Approx. 1 second
Filters (mounted)	1 dark + 7 science (Y, J, H, K <sub>s</sub> , + TBD)

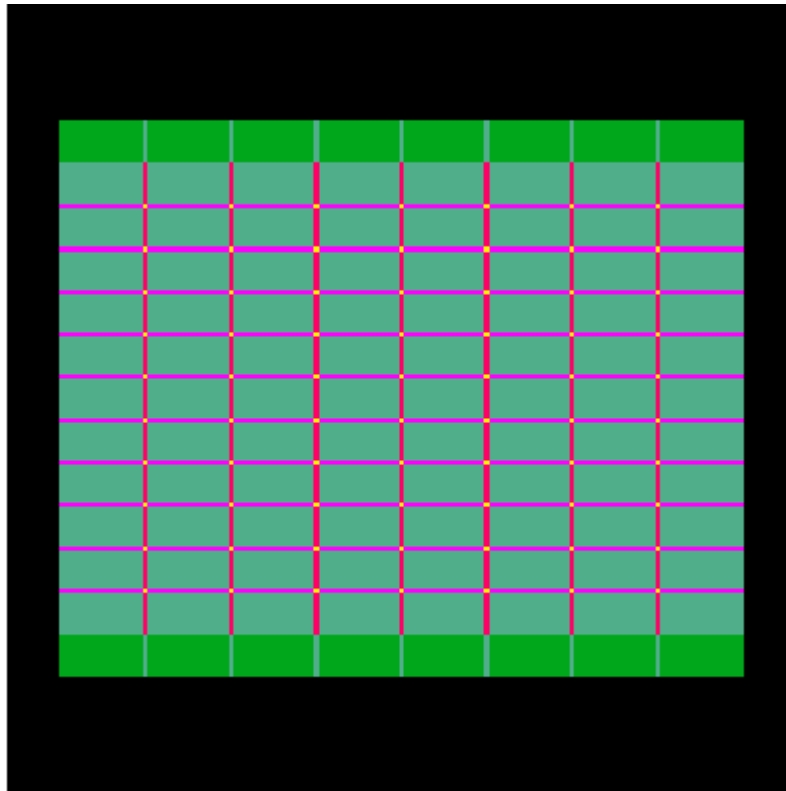
**Table 2-1: VISTA and VIRCAM baseline system parameters**

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**Figure 2-1: Layout of the 16 science detectors in the focal plane. Circle is 1.65 deg in diameter. Also shows “effective locations” (via pickoff mirrors) seen by the autoguiders (AG) and the LOWFSs.**

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**Figure 2-2: Exposure time map for a filled tile of 6 pawprints (no jittering). Dark green = 1, light green = 2, magenta = 3, red = 4, yellow = 6, in units of the single-pawprint exposure time.**

## 2.2 Observing Considerations

The hardware clearly places certain constraints on operational modes, though not many, as the system has been designed to be fairly flexible. Since there is only one moving part in the camera (the filter wheel), the telescope and instrument configuration is primarily specified by the pointing direction (RA and Dec), the Cass rotator angle and the filter.

The Cass rotator has a travel of 540 degrees so the position angle of the focal plane with respect to the sky may be chosen freely (the default will probably be the long (X) axis aligned East-West). Note that the focal plane assembly, autoguiders and LOWFSs are 180-deg symmetric, so if desired one can observe a field at two camera angles 180° apart while re-using the same guide stars.

The most obvious constraint is the layout of detectors on a  $4 \times 4$  rectangular grid with gaps of 90% of a detector width in  $x$  and 42.5% in  $y$ . This requires observing 6 “pawprints” to give a filled “tile”. Each pawprint may comprise many exposures at different jitter or microstep positions, as desired for optimal flat-fielding and/or sampling. These moves are user-selectable and not “quantized”, but should be limited in size. This is because after tiling moves, the overlaps between adjacent pawprints have a width of  $\sim 5\%$  of a detector or 30 arcsec. Therefore jitter moves within a pawprint must not exceed  $\pm 15$  arcsec away from a “central” jitter position to

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avoid underexposed stripes in the final tile. Figure 2-2 shows an exposure time map for a filled tile that is composed of six pawprints.

Due to field distortion, if we want to use microstepping, the constraint is more stringent. The radial plate scale in arcsec/pixel is 2.4% larger at the field corner than the centre, so e.g. a microstep of 9.9 pixels at the centre corresponds to 10.14 pixels at the field corner. Therefore, microstep offsets must be limited to not more than  $\sim 3$  arcsec.

Ultimately if one wants both microstepping and a jitter size  $\geq 3$  arcsec, separate nested loops are required. This is fine for deep exposures but may preclude microstepping for shallow surveys.

## 2.3 *Active Optics and Guiding*

The VISTA active optics system is largely “transparent” to science observing. There is a closed-loop low-order wavefront sensing system (controlling focus and collimation of M2), and an open-loop (lookup table) high-order system controlling the figure of M1 via 84 axial force actuators.

There are two identical fixed autoguider and LOWFS units at opposite sides of the FOV, each fed by a pickoff mirror and a fixed filter (roughly I-band). Each autoguider has one frame-transfer CCD chip giving an  $8 \times 4$  arcmin field, although only one will be in use at a time (whichever has a brighter star).

The LOWFSs have large enough field of view ( $8 \times 8$  arcmin) to contain a usable star for almost all telescope pointings, so should not impose significant pointing constraints, and they usually add no “overhead” since their exposures should start after and finish before the science integrations. Use of the LOWFSs imposes a minimum time between jitter moves of  $\sim 30$  sec since they have to complete an exposure with adequate SNR in between consecutive jitter moves. If it is essential to jitter more often than once per 30 sec, this can be done using open-loop M2 control, though a slight loss of image quality may result.

The one exception is after a telescope slew giving a large ( $\geq 10^\circ$ ) change in altitude. Then there may be a need for a 30-sec pause for one LOWFS cycle to complete and update the M2 position before science observing re-starts.

Given the above sensor fields, generally a “jitter” movement of  $\leq 15$  arcsec will re-use the same guide and wavefront sensor stars by simply offsetting the selected readout window in software, whereas a “tiling” offset of 5-10 arcmin will almost always require different guide and LOWFS stars to be selected after the move. Checking and acquiring the new guide star will impose a short overhead of  $\sim 1$  second per tiling move.

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## **2.4 Filters**

The filter exchange mechanism is a large wheel of 1.37m diameter (actually an annulus with a fixed pillar through the centre) with 8 main positions for 1 dark and 7 science filters. Filter exchange time is expected to be ~ 15-45 sec depending on angle. This is clearly longer than that for a jitter or tiling telescope move, so it is generally more efficient (and gives better sky subtraction) to complete a tile in one filter, then change filters and repeat.

Filters will be ordered in the wheel so that the detectors do not see an increased background during filter change. Due to non-uniform temperature across the wheel, a filter change is likely to cause a small warming of the detectors, but this should be corrected by the temperature servo system, so the temperature rise should be  $\leq 0.1\text{K}$  for a few minutes after the change. With a wheel temperature  $< 110\text{K}$ , photon emission from the wheel itself should always be negligible.

The wheel also contains “mini-filters” in the V-shaped sectors in between the large science filters. These mini-filters cover only a small fraction of the focal plane, and, with the exception of the HOWFS beam splitter, are primarily for engineering use.

## **2.5 Survey Efficiency**

### **2.5.1 Introduction**

VISTA’s overriding purpose is to conduct surveys efficiently. To expedite this aim, an Exposure Time Calculator (ETC) will be provided to ensure observations are timed optimally for the particular science objectives, and observing templates must be designed to maximise speed, but without compromising the scientific integrity of the data. [RD6] discussed the observing efficiency budget for system design purposes. To aid in determining efficiency of observing strategies and of observing templates, this subsection indicates the typical expected overheads in the operation of the VISTA/VIRCAM in terms of the time needed for each change of state/movement of the system between exposures. Of course the effect of these overheads on survey efficiency is particularly strong for surveys involving short exposures.

### **2.5.2 Exposure Time Calculator**

An ETC will be specified in a separate document [RD8], which sets out the relationship between astronomical requirements (magnitude limits, signal/noise etc.) and observational variables (seeing, sky brightness etc.). The main task of the ETC is to evaluate the exposure time required to reach a given signal-to-noise for a given set of source characteristics, atmospheric conditions, filter and tiling strategy. The ETC will also allow the equivalent signal-to-noise to be computed for an input exposure time. To aid in construction of efficient OBs, the ETC will also calculate the elapsed time and the observing efficiency, taking into account the internal overheads involved in making a single tile in one filter.

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### 2.5.3 Moving to a new Tile

The time to go to a new tile will depend on how far away it is in altitude and azimuth from the current position, and on the zenith distance. As for any alt-azimuth telescope at VISTA's latitude one wants to minimise presets between objects with Dec  $< -24^\circ$  to Dec  $> -24^\circ$  and vice versa. Both alt and azimuth can accelerate at  $0.5^\circ/\text{s}^2$  and max angular velocity is  $2^\circ/\text{s}$ , so it takes a 4-sec ramp-up to reach max angular velocity (and covers 4 deg in those 4 sec). The Cassegrain rotator is faster ( $1^\circ/\text{s}^2$  and  $3.6^\circ/\text{s}$ ) so will hardly ever be the limiting overhead.

The "worst case" preset is a  $270^\circ$  azimuth move from SE to NE which has to go the long way round via W due to the cable wrap, and which will take  $\sim 140$  seconds. These situations should be avoided, if at all possible, during scheduling.

A small preset of  $2^\circ$  on-sky, in the worst case, can require a  $\sim 60^\circ$  azimuth move if alt =  $88^\circ$ . Fortunately a more "typical" case at alt =  $60^\circ$  only requires a  $\sim 4^\circ$  azimuth move. Assuming an acceleration of  $0.5^\circ/\text{s}^2$  for 2.82 sec followed by equal and opposite deceleration at same rate, this will take  $\sim 5.84$  seconds (a smoother algorithm may take a bit longer so  $\sim 10$  sec is a more reasonable estimate). If the  $2^\circ$  is mostly in Altitude it will be somewhat quicker.

In the best case the time to go to a new tile will be comparable to that to change to an adjacent filter or to offset, but in general it will be longer.

### 2.5.4 Changing Filter

Sec 4.3.3.2 of [RD4] specifies the filter exchange time for an adjacent filter as  $< 25\text{sec}$  although the expected time is  $\sim 12$  sec. The filter exchange time to any filter is specified as  $< 60\text{sec}$  and the expected time is  $\sim 40$  sec.

### 2.5.5 Moving to a new Pawprint, Jitter, Microstep

- The time to offset to another pawprint of the same tile (5-10') will be  $\sim 10\text{sec}$ .
- The typical time to move a jitter step ( $< 30''$ ) within a pawprint will be  $\sim 4\text{sec}$ .
- The typical time to move a microstep ( $< 3''$ ) within a jitter will be  $\sim 2\text{sec}$ .

Although the LOWFS operates in parallel with science observations up to 30sec integration is required for adequate S/N in the 99% faint case. In all cases, including the brighter cases, averaging over several LOWFS exposures will be needed because the atmospheric errors (which are independent of star brightness) go as  $1/\sqrt{\text{Time}}$ . Care will need to be taken to minimise overheads associated with LOWFS, especially if exposures are short, or if LOWFS would start at the end of science integrations.

### 2.5.6 Exposures

The minimum single integration time is equal to the readout time of approximately 1s. The way the exposure time is made up of integrations may be filter and sky brightness dependent, for example the time for sky to half-fill the wells is  $\sim 8\text{-}12\text{s}$  (H and  $K_s$ ), longer for other filters. The minimum sustainable duty cycle for exposures is 10

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seconds. The overhead for one exposure of  $N$  co-added integrations is expected to be  $(N+1) \times (\text{readout time})$  seconds, e.g. a typical 60s exposure comprising 6 co-added integrations will take approximately 67s elapsed time. How this translates into designing efficient survey practice, trading off instrument and telescope overheads against sky condition and science aims, is beyond the remit of this document.

## 3 Summary of Science Requirements

### 3.1 Introduction

The following specific requirements, whilst placed on the end-to-end VISTA system, indicate the accuracies expected from the calibration pipeline. These have been outlined in detail in the VISTA Science Requirements Document (SRD) [RD3]. In what follows we append a specific reference to the section of the SRD from which the requirement is drawn.

### 3.2 Astrometric Accuracy

- [from SRD 4.5.1/1] For sources bright enough so that there is negligible centroiding error due to photon noise, the end-to-end system shall deliver differential astrometric accuracy of  $0.1''$  RMS over the whole of the field covered by the IR mosaic to an airmass of 2.
- [from SRD 4.5.1/2 and 4.5.1/4] For sources bright enough so that there is negligible centroiding error due to photon noise, the end-to-end system shall deliver differential astrometric accuracy of  $\leq 0.03''$  within the field covered by each individual IR detector to an airmass of 2.
- [from SRD 4.5.1/3] For sources bright enough so that there is negligible centroiding error due to photon noise, the end-to-end system shall deliver absolute astrometric accuracy of  $\leq 0.3''$  over the whole of the field covered by the IR mosaic to an airmass of 2.

### 3.3 Photometric Accuracy

It is assumed that a well defined grid of standard stars will be available on the southern sky.

- [from SRD 4.6.1/1] The end-to-end system should not preclude achieving absolute photometric accuracies (in J, H and  $K_s$ ) of  $0.02^m$  (with a goal of  $0.01^m$ ) on sources bright enough so there is negligible photometric error due to photon noise, over the survey region.

### 3.4 Non operational Detectors

- The pipeline shall be capable of operating normally if a subset of the detectors is missing or non-functional.

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## 4 Data-Flow System Requirements

### 4.1 *Basic Operation*

VISTA will adhere to a limited but flexible set of observing templates, designed to use the instrument to its maximum efficiency and to enable calibration. Unlike other ground-based telescopes, where a few nights at a time are allocated via a competitive process to conduct one-off experiments, at least 75% of VISTA's time will be dedicated to coherent long-term surveys.

The observing system will be capable of performing overlapped observations suitable for the construction of filled-in tiles, although such further image combination is beyond the scope of the pipeline.

### 4.2 *Pipeline Requirements*

#### 4.2.1 Outline

Broadly speaking there are four separate pipeline requirements:

- 1) Removal of Instrumental Signature
- 2) Astrometric Calibration
- 3) Photometric Calibration
- 4) Those that generate Quality Control measures

The pipeline will reduce all data as far as possible, even when a template has been aborted.

#### 4.2.2 Instrumental Signature Removal

The aim of instrumental signature removal is to produce, as near as possible, an image as though it were taken with a perfect, linear, blemish-free camera. The images arrive from the DAS having already been reset-corrected. Thereafter the VISTA pipeline is responsible for providing the following operations:

- **Dark Correction:** This is needed to subtract out the thermal dark current and the reset anomaly from each frame.
- **Linearisation:** Detector outputs (including amplifier and ADC) are generally non-linear. This operation has to reduce the non-linearity to acceptable levels, taking into account the complexity involved in the readout process. This effect requires specific characterisation and long-term monitoring.
- **Gain Correction:** This is required to remove the following multiplicative effects:
  - pixel-to-pixel quantum efficiency variations
  - large scale variations, mostly due to vignetting
  - global gain variations between detectors

Observations of a uniformly illuminated far-field are used to model these effects. The resulting 'flat-field' is used to normalise the target observations.

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- **Background Correction:** The sky in the infrared is variable both temporally and spatially over short intervals. Some broad passbands also have contributions from sky fringing and thermal emission from dust on the camera optics. Background correction is required to reduce these effects to acceptable levels.
- **Electrical Crosstalk:** Each of the 16 VIRGO detectors will be read out using 16 adjacent channels. The signal from one channel can interfere with the signal on other channels or detectors that are clocked out at the same time. The crosstalk may be negligible, but needs to be specifically characterised prior to, or during, commissioning and monitored thereafter. The effect will be characterised and removed via a crosstalk matrix of 256x256 entries.
- **Persistence:** Images of objects from previous exposures may remain on a detector for some time after the initial image was taken and possibly spread into adjacent pixels. The rate of decay of such images and their possible adjacency effects require characterising during commissioning and monitoring thereafter. Persistency effects, if present, then need to be reduced as much as possible in science frames.
- **Non-uniform illumination:** Although the flat field normalisation described previously should take out all of the large scale variation in sensitivity, in practice this may not be so. As with any camera, VIRCAM may have scattered light present. This will impose a smoothly varying structure on the otherwise uniform flat-field illumination and hence will result in a variation in the photometric zeropoint across the detector. This requires characterising and mapping to a suitable level of accuracy.
- **Bad pixels:** Bad pixels (including hot pixels) are to be flagged from the beginning of the pipeline processing using confidence maps. When the exposures from a jitter sequence are combined into a single image, the effect of bad pixels must be reduced to minimal level.
- **Under-sampling:** In times of exceptional seeing, the point-spread function will be under-sampled. If this occurs, then observations that are microstepped for interleaving may be required. This involves taking a group of four exposures, each of which is offset by an integer number of pixels, plus 0.5. OBs will have been prepared for programs requiring such high resolution; the data frames will be identified as such by a FITS keyword, and the pipeline should then interleave the four exposures into one frame with twice the pixel resolution, thereby recovering some of the lost spatial resolution.

#### 4.2.3 Astrometric Calibration

Routine astrometry of VISTA science data is required for all science data. Any astrophysical exploitation of the data depends on being able to locate sources precisely (in particular for follow-up observations) and to register multi-wavelength images and maps. The astrometric calibration will be manifested in the form of a FITS-standard World Coordinate System (WCS), in the International Coordinate Reference System (ICRS).

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The observing system will write an initial WCS derived from knowledge of the focal plane and camera geometry, as well as the pointing information provided by the TCS. The accuracy of the initial WCS is required to be  $\leq 5''$ , but is expected to be  $\leq 2''$  [RD3]. During pipeline processing, a precise WCS must be derived for the output frame (which in general will be a combined image) by referring detected point-sources to the 2MASS or USNOB catalogues. The accuracy of the precise WCS is required to be  $\leq 0.2''$ , but is expected to be  $\leq 0.1''$ .

#### **4.2.4 Photometric Calibration**

In order to fulfil the science requirements, sufficient photometric standards must be observed each night to enable the pipeline to produce photometric zero points and extinction measures. Non-photometric nights will be flagged via error estimates in this calibration.

The photometric calibrations, including extinction measures, which describe the transformation between internal (instrumental) fluxes to magnitudes on the VISTA photometric system, must be recorded for later use. It is assumed that a suitable catalogue of standards will exist, which may have to be generated in a special observing programme. Some secondary standard fields for VISTA will be defined as part of the observing programme for WFCAM (but this does not imply that VISTA is dependent on WFCAM operations).

#### **4.2.5 Quality Control and Data Characterisation**

Quality measures must be made and recorded at all stages of the reduction procedure including, but not limited to, QC-1. Post-pipeline trend analysis should include comparing calibration frames with master frames to look for spatial and temporal variations. Science data must be examined for uniformity of overlap areas, consistency of PSF across detectors and numbers of ‘negative’ in addition to ‘positive’ spurious images. The offset from initial to final WCS provides a measure of the telescope acquisition performance, whereas trailed or distorted PSFs can be an indication of poor tracking or other problems. Variations in the photometric zero point and/or extinction coefficient can be used to flag poor observing conditions.

A more comprehensive list of data quality indexes to be used is described in the Data-Reduction Specifications document [RD2].

### **4.3 Data Rate and Volume**

The unprocessed data volume (including FITS headers) is 268.6 MB/exposure. The maximum data rate VIRCAM is designed to handle is one exposure every 10 sec over a night of 14 hours i.e. 1350 GB per operational night. A more usual expectation for a typical high-volume night given overheads is one exposure every 20 sec for 13 hours i.e. 630 GB per operational night. A median night (i.e. typical observing cadence) is estimated to be 1 exposure every 60 sec for 13 hours, i.e. 210 GB per operational night. Although the details will depend on the actual surveys awarded time, and the

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details of their actual observing strategies, a reasonable assumption is that a mean (over time) operational night will involve  $\sim 75\%$  median nights (210 GB/night) and  $\sim 25\%$  high-volume nights (630 GB/night) leading to a mean data rate of 315 GB per operational night. Note that the distinction between median and mean is very important here. The mean is  $1.5\times$  higher than the median since some nights (e.g. shallow surveys) will have  $\sim 3\times$  the median data rate, but most nights will not be much less than the median.

#### **4.3.1 Maximum Nightly Raw Data Rate**

The DFS infrastructure (local storage, transmission to Europe and the pipeline) should be able to handle typical high-volume data nights of 630 GB per operational night (shallow survey), with a goal of handling the maximum VIRCAM design rate of 1350 GB per operational night (intense repeat observations on a single field, an uncommon but not impossible scenario).

#### **4.3.2 Mean Nightly Raw Data Rate**

The DFS infrastructure should expect to handle a mean raw data rate of 315 GB per operational night.

#### **4.3.3 Typical Annual Raw Data Volume**

Assuming 10 nights engineering time per year and 15% loss of the remaining 355 days to weather gives data for 300 operational nights a year. At 315 GB per operational night the resulting yearly raw data volume is 95 TB. (Note that dividing this volume by 365 gives a smoothed rate of 260 GB per elapsed calendar day).

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## 5 Survey Planning

### 5.1 Introduction

Unlike most other ground based telescopes, where a few nights at a time are allocated via a competitive process to conduct one off experiments, at least 75% of VISTA's time will be dedicated to a set of coherent long term surveys and most of the remaining 25% will be used for Principal Investigator-led surveys. A typical multiband survey would cover a certain area (which may or may not be contiguous), would be observed to a uniform depth in several filters and would possibly be done with some repetition to pick up variability. Such a survey will normally be the result of the combination of many observations made over many nights and several such surveys will probably be running concurrently.

A typical survey consists of a number of filled tiles and involves observing:  $F$  filters \*  $T$  tiles \*  $P$  pawprint positions/tile \*  $J$  jitter positions/pawprint \*  $M$  microstep positions/jitter \*  $E$  exposures/microstep. This produces a total of  $F*T*P*J*M*E$  raw exposures to be saved in the archive.

There are 4 filters delivered with VISTA so initially  $F$  can be 1 to 4. If further filters become available,  $F$  can be up to 7. In any situation where darks may need to be taken interleaved with sky exposures (for example if there are problems with unstable reset anomaly) the cold blocker can be considered another filter. The number of tiles,  $T$ , in a survey will depend on the areas to be covered and the coverage strategy. The default method of making a tile requires  $P=6$ .  $J=1$  means no jittering and  $M=1$  means no microstepping.  $E = 1$  usually (i.e. all the required exposure time is taken in one exposure). But one might want to divide the required exposure time into several sub-exposures (e.g. to check for time-dependence of sky), so  $E$  could be  $> 1$ .

The pipeline is not expected to produce complete calibrated surveys, but to calibrate the data as it is acquired at the summit, and from each whole night at Garching. The unit of sky area that the PIPELINE will calibrate is a pawprint in a single filter observed in a contiguous block of time. It is recognised that in general the pawprint will be a component of a tile, that complementary pawprints may exist in other filters and that the pawprint may have been observed multiple times on the same or different nights for stacking or variability. It is not within the remit of the PIPELINE to combine the pawprints. However the calibration of the individual pawprints should be carried out with a view to providing the necessary calibration information to enable such combinations to be made by others.

### 5.2 Nesting of Component Observation Loops of a Survey

The component observations of a survey (filters  $F$ , tiles  $T$ , pawprints  $P$ , jitters  $J$ , microsteps  $M$ , and exposures  $E$ ) can in principle be nested in various orders, subject to some restrictions, such as the innermost loop always being  $E$ . Different nestings require different observing templates, and it is necessary to choose a suitable subset of the possible nestings, without precluding the later addition of other templates should a

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use for them be identified. Thus the observing templates are classified and described in the Calibration plan [RD1] in terms of the nesting of the component loops.

Although it is not strictly necessary to complete all pawprints of a tile before moving to the next tile it will generally be efficient to do so, thus it is assumed that a pawprint, P, is always nested within a tile, T, since a tile is always composed of a set of pawprints. Survey nestings whose innermost loops are not JME are assumed, on grounds of efficiency, not to be needed at present.

Using a shorthand (based on the order of nesting of the loops for the 6 components F,T,P,J,M,E with the order of the letters indicating increasing nesting of the loop as one reads to the right) the three remaining nestings would be:

- **FTPJME** — Complete all tiles in one filter, change filters and repeat the tile sequence. The observation loops would look something like this (where Check/Set means check if the system is already in the demanded state, or position, and if it is not change state, or move position):

For each demanded filter position (1 to F)

For each tile 'centre' position (1 to T)

Preset to tile 'centre' position

Check/Set IMAGING mode

Check/Set camera PA in parallel [default +X axis to +RA]

Check/Set demanded filter in parallel

For each pawprint (steps 5-10') (1 to P)

Check/Offset telescope to pawprint central position

Acquire guide star

LOWFS on two stars in parallel (for minimum of 30s)

For each jitter-position (1 to J)

Move telescope (steps <30", same guide star)

For each microstep (1 to M)

Move telescope (steps <3", same guide star)

For each exposure (1 to E)

Make exposure

Next exposure

Next microstep

Next jitter

Next pawprint

Next tile

Next filter

- **TFPJME** — Complete each tile in all filters before starting on the next tile in the sequence. This would have the following observation loops:

For each tile 'centre' position (1 to T)

Preset to tile 'centre' position

Check/Set IMAGING mode

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Check/Set camera PA in parallel [default +X axis to +RA]  
 Check/Set first filter in parallel  
 For each demanded filter position (1 to F)  
     Check/Set demanded filter in  
     For each pawprint (steps 5-10') (1 to P)  
         Check/Offset telescope to pawprint central position  
         Acquire guide star  
         LOWFS on two stars in parallel (for minimum of 30s)  
         For each jitter-position (1 to J)  
             Move telescope (steps <30", same guide star)  
             For each microstep (1 to M)  
                 Move telescope (steps <3", same guide star)  
                 For each exposure (1 to E)  
                     Make exposure  
                 Next exposure  
             Next microstep  
         Next jitter  
     Next pawprint  
 Next filter  
 Next Tile

- **TPFJME** — Complete each pawprint of the tile in all filters before starting on the next pawprint of the tile. This would have the following observation loops:

For each tile 'centre' position (1 to T)  
     Preset to tile 'centre' position  
     Check/Set IMAGING mode  
     Check/Set camera PA in parallel [default +X axis to +RA]  
     Check/Set first filter in parallel  
     For each pawprint (steps 5-10') (1 to P)  
         Check/Offset telescope to pawprint central position  
         Acquire guide star  
         LOWFS on two stars in parallel (for minimum of 30s)  
         For each demanded filter position (1 to F)  
             Check/Set demanded filter in  
             For each jitter-position (1 to J)  
                 Move telescope (steps <30", same guide star)  
                 For each microstep (1 to M)  
                     Move telescope (steps <3", same guide star)  
                     For each exposure (1 to E)  
                         Make exposure  
                     Next exposure  
                 Next microstep  
             Next jitter  
         Next filter  
     Next pawprint  
 Next Tile

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Each of these three alternatives would produce the same number of output files, but the observing overheads would not be the same, and in variable atmospheric conditions the relative limiting magnitudes achieved in each filter would be different. Furthermore the time baseline over which colours were calculated would be different.

(There are further possible alternatives if we allow the filter F to change within the J or M loops, or relax the restriction that JM loops be within P loops, or that M loops be within J loops, or that ME must be in the inner loop.) Another example where the sequences would be different is a wide shallow survey compared to a narrow deep survey.

This illustrates the fact that surveys with different aims may want to use different observing sequences, as well as exposure times, and that there may be tensions between a sequence that is preferred and another that is more efficient. The ETC tool will provide the time for each allowed observing sequence input to be computed and a quantitative comparison made.

### **5.3 Observing templates**

The VISTA pipeline deals with calibrating nights of data, not producing whole surveys, whilst recognising that the nights form part of whole surveys. Therefore the templates that are defined in the Calibration Plan [RD1] are those that are appropriate for observing single pawprints, or for observing the pawprints necessary to complete a tile during a single night.

Templates are defined in the Calibration Plan [RD1] only for those observing sequences that are perceived as most likely to be used, not for every template that is possible. However, it is important that the observing templates allow the necessary flexibility in designing surveys to enable each of the Design Reference Surveys given in [RD5] to be carried out, together with, any further Design Reference Surveys that may be identified before.

### **5.4 Survey Definition Tool**

Many VISTA surveys will be large multi-night to multi-year programmes and the resulting requirements on defining the component observations of the Surveys were given in [RD10]. Guided by this, [RD9] defines the details of the Survey Definition Tool which:

- Calculates coordinates for VISTA tiles to fill given areas of sky
- Displays survey area covered in tiles/pawprints
- Selects guide and aO stars for each pawprint
- Creates OB for each tile based on a 'parent OB' (an SDT term).

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## **5.5 Survey Scheduling**

The scheme by which the component observations of these large surveys are best scheduled will need to be carefully considered, including the scheduling issues raised in [RD10]. As the functionality of the current version of the Paranal observing queue scheduler imposes some undesirable (for VISTA) scheduling restrictions ESO are in the process of defining ‘Execution Principles and Requirements on Preparation and Scheduling Tools’ which should be more appropriate for surveys, taking into account many of the issues of concern to VISTA [RD10]. Such questions, and potential solutions, are outside the remit of the VISTA Data Flow System deliverables to ESO, although it remains important for VISTA that these issues are resolved. The present document is therefore restricted to considering how best to make the observations scheduled for any given night, regardless of how they were selected.

## **5.6 Survey Progress Tool**

A Survey Progress Tool is also covered in [RD9] which currently specifies:

- Overall visualisation. Similar to the survey area display of the Survey Definition Tool: plots tiles in a colour indicating the status of the corresponding OB (e.g. ‘done’, ‘not done’ etc.).

Two further items needed to follow survey progress require further discussion with ESO and are:

- Progress data files and their visualisation
- How such progress output can feed back into survey scheduling

## **5.7 Partial Failure Mode Contingency Planning**

It must be expected that the system will occasionally fail in ways which do not preclude some kind of valuable continued operation. While not every contingency can be planned for, the response to some likely scenarios can be sketched.

### **5.7.1 Bad Pixels**

A significant number of bad pixels are confidently expected; their elimination from the final data drives the jittering observational strategy and the essential incorporation of confidence maps in the reduction procedures.

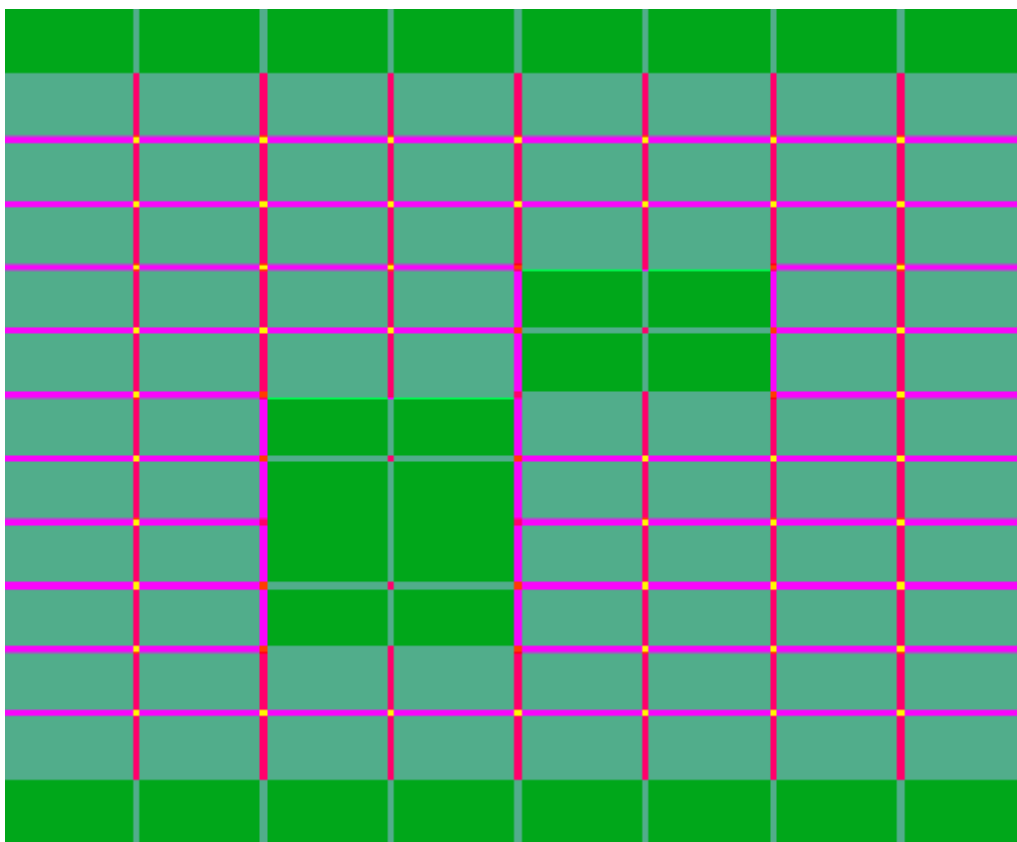
### **5.7.2 Dead Detectors**

It is possible that one or more of the 16 detectors ceases to function during service. Immediately this happens, observing should continue regardless. If efficient sky coverage is the main science driver, irrespective of gaps in the data, then the default strategy would be to continue with the programmed tiling, since the generated confidence maps monitor the effective exposure of each pixel and can be used (automatically) to mitigate the science impact. For other cases, because there are 16! combinations of failures, the remaining pattern of functional detectors would be examined, and a strategy worked out to most efficiently fill in sky coverage. However, a few characteristic patterns can be thought about:

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- 1 or more chips fail in an edge row. This leaves an intact 4×3 array which could be used to define new field centres.
- 1 chip fails in central 2×2 square. 180° rotation during tile observation would provide coverage.
- An extreme case of multiple chip failures. It might involve an engineering change to move good detectors from the outside to the centre region of the focal plane.

In any case, the reduction pipeline shall continue processing as specified in 3.4. An example of how a failure of a central chip might be ameliorated is shown in Figure 5-1.



**Figure 5-1** A tile composed of six pawprints, in which one of the central detectors is unservicable. The central Y-offset pawprints are observed at 180°. Compare with Figure 2-2.

### 5.7.3 Missing Guide and LOWFS Stars

VISTA ideally requires 3 guide/AO stars for each pawprint, 1 guide star and 2 LOWFS stars, all in different sky areas and hence distinct. These 3 stars will be common to all microstep/jitter positions for a pawprint, but each new pawprint will require 3 new stars.

There are various possible failure cases. However in most cases these can be handled with minimal impact on image quality:

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- (i) failure to find a catalogue star at time of OB preparation. This should be rare since a mean of  $> 5$  useful stars per sensor is expected at the Galactic poles, and many more at low Galactic latitude;
- (ii) a pre-selected star turning up bad when observed (e.g. a close binary, asteroid, catalogue error etc);
- (iii) poor weather meaning that a normally usable star has insufficient SNR at the actual observing time;
- (iv) hardware failure of one or more sensors;
- (v) or combinations of these.

The survey planning tool document [RD9] explicitly defines how these situations will be dealt with.

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